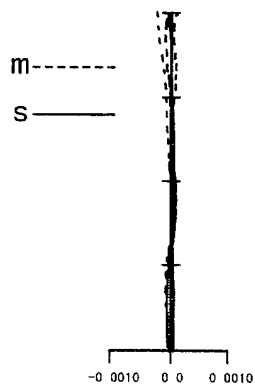
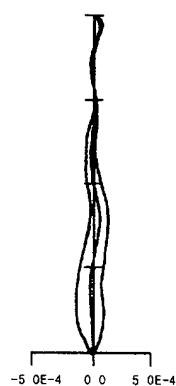


SPHERICAL
ABERRATION



ASTIGMATISM



DISTORTION (%)

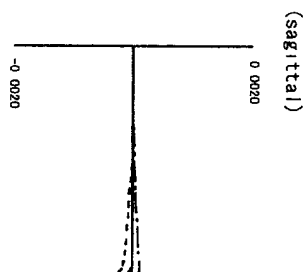
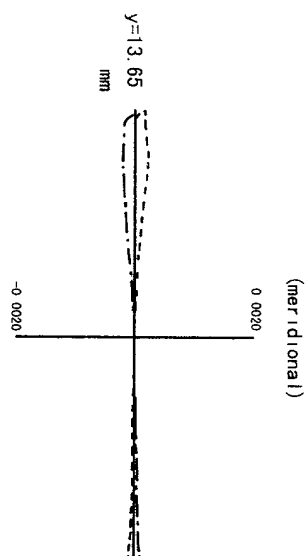
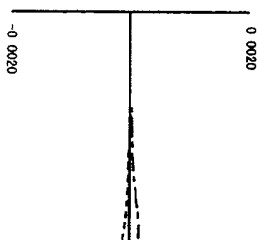
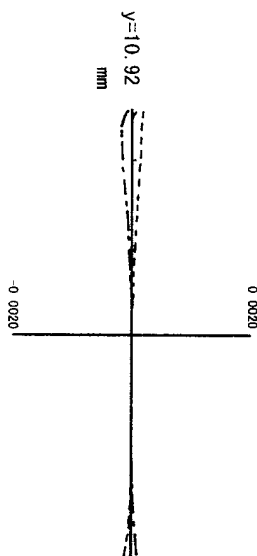
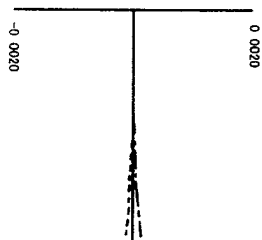
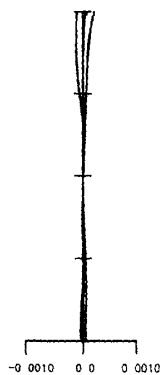
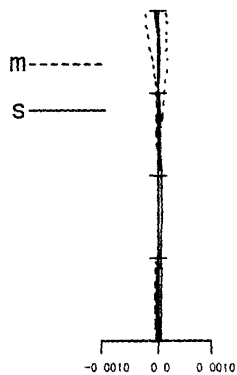


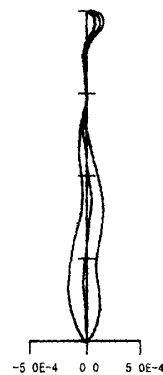
FIG. 35



SPHERICAL
ABERRATION



ASTIGMATISM



DISTORTION (%)

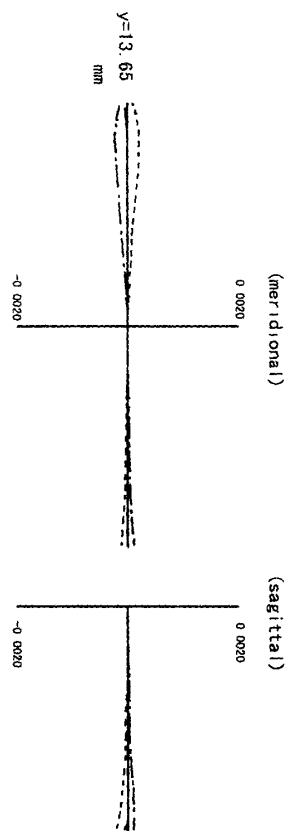
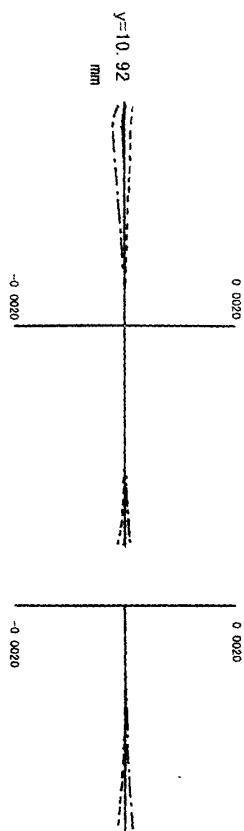
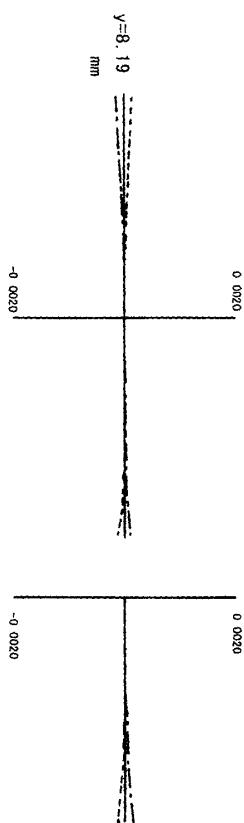
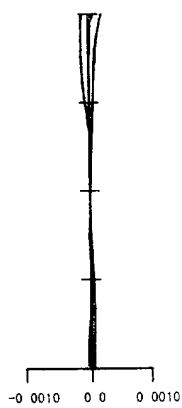
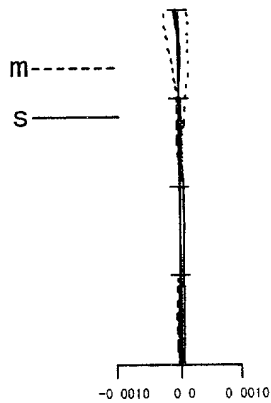


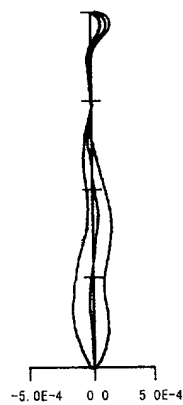
FIG. 36



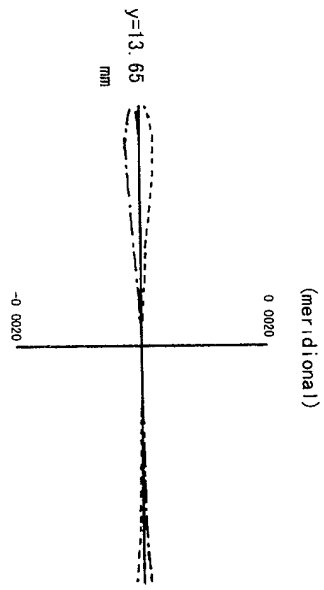
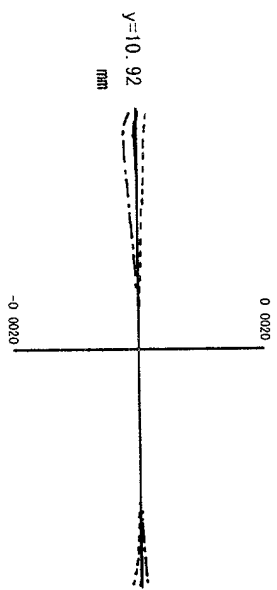
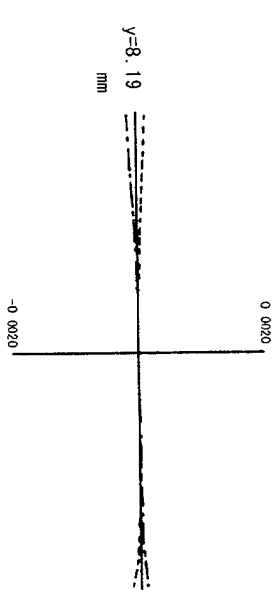
SPHERICAL
ABERRATION



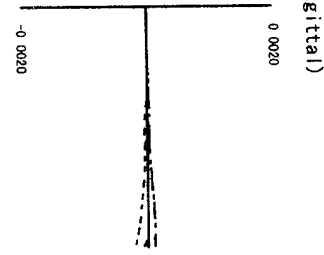
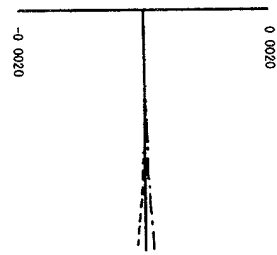
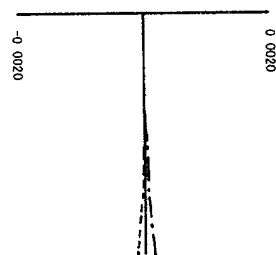
ASTIGMATISM



DISTORTION (%)

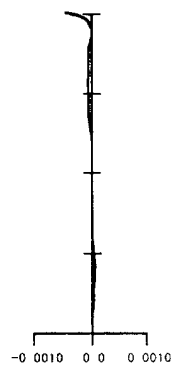


(meridional)

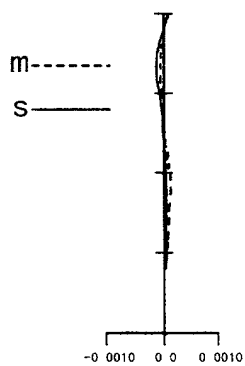


(sagittal)

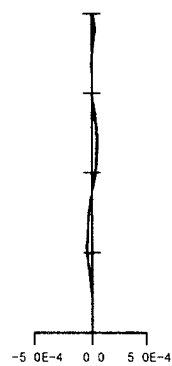
FIG. 36



SPHERICAL
ABERRATION



ASTIGMATISM



DISTORTION (%)

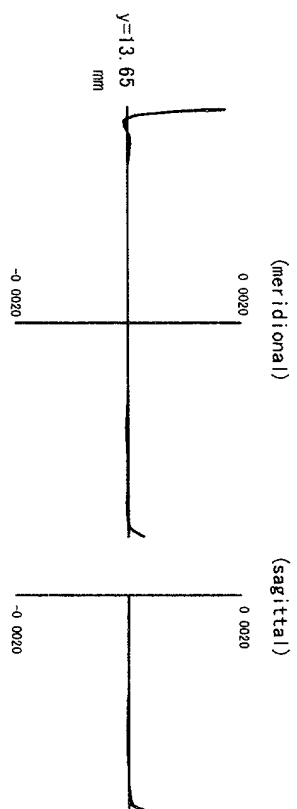
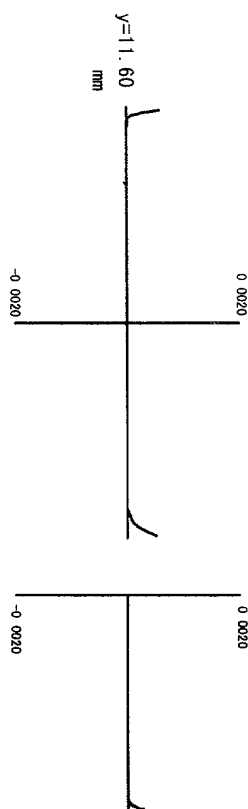
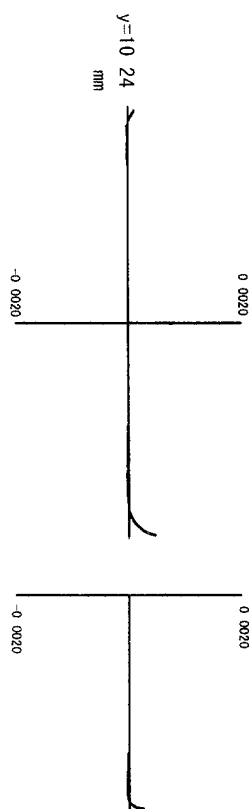
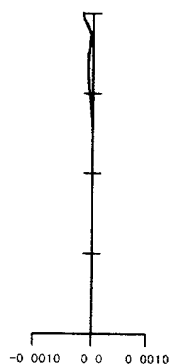
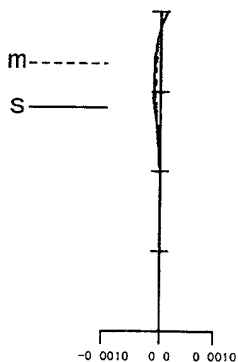


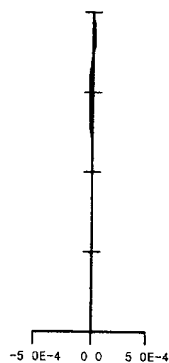
FIG. 37



SPHERICAL
ABERRATION



ASTIGMATISM



DISTORTION (%)

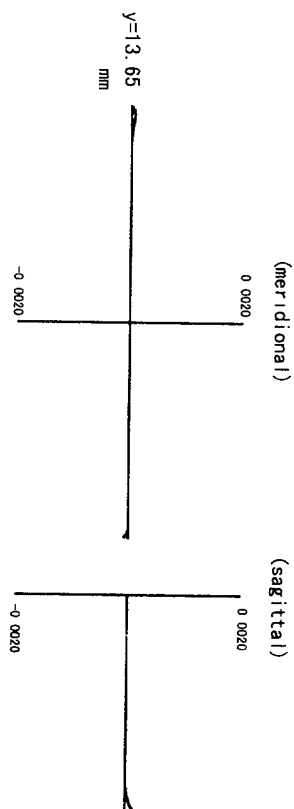
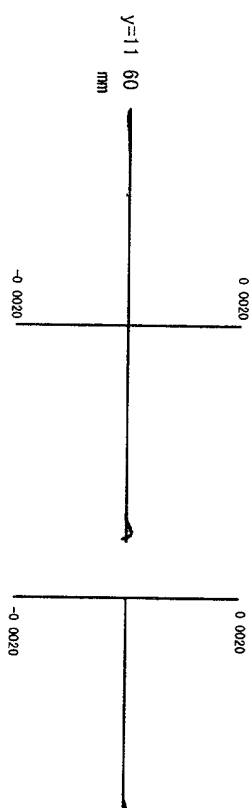
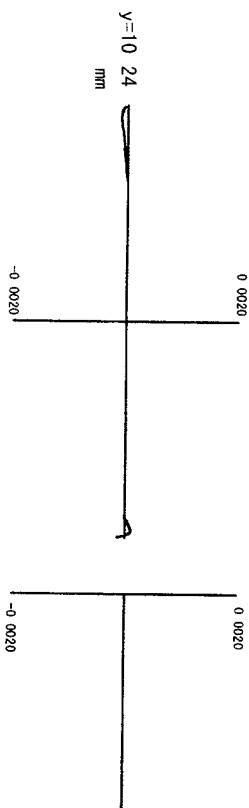
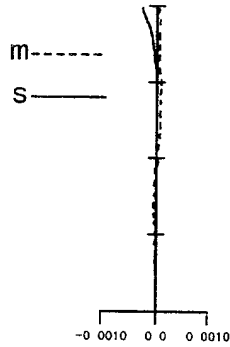


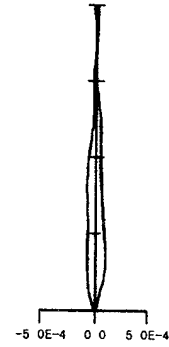
FIG. 38



SPHERICAL
ABERRATION



ASTIGMATISM



DISTORTION (%)

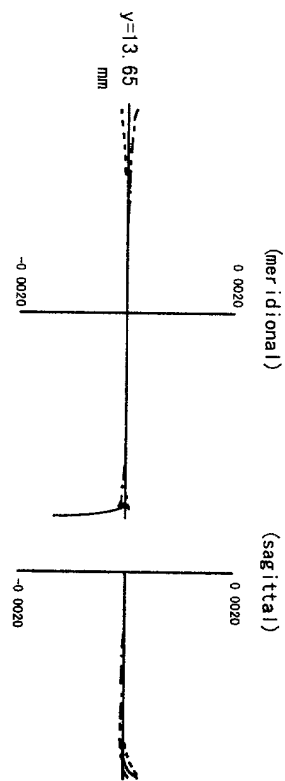
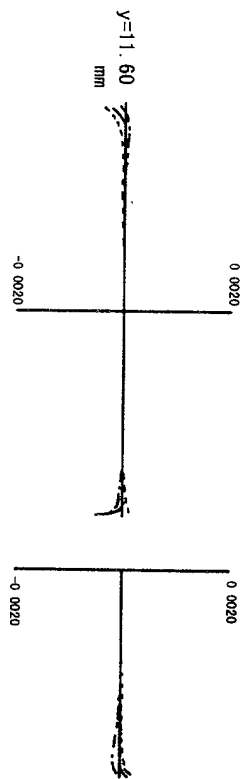
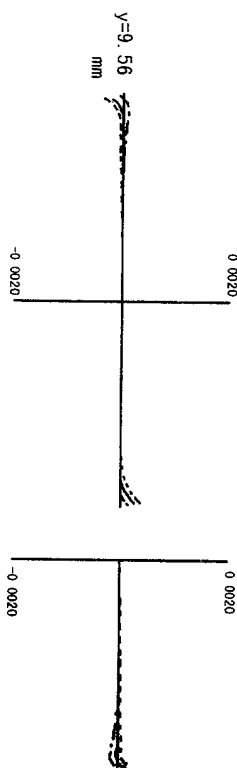
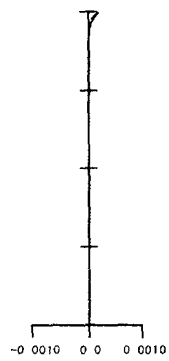
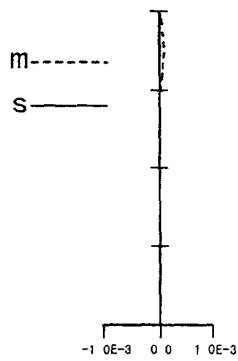


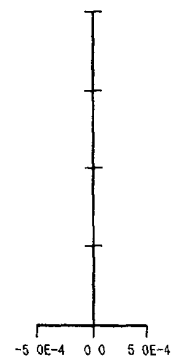
FIG. 39



SPHERICAL
ABERRATION



ASTIGMATISM



DISTORTION (%)

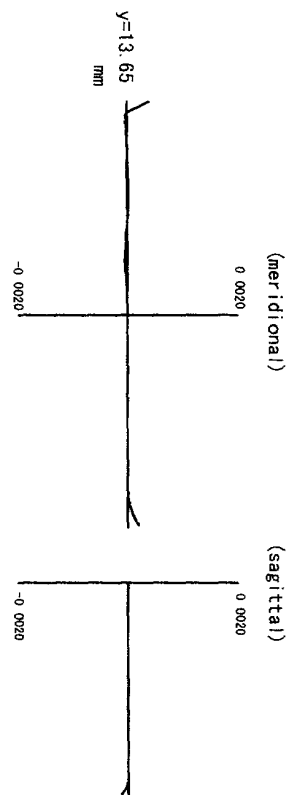
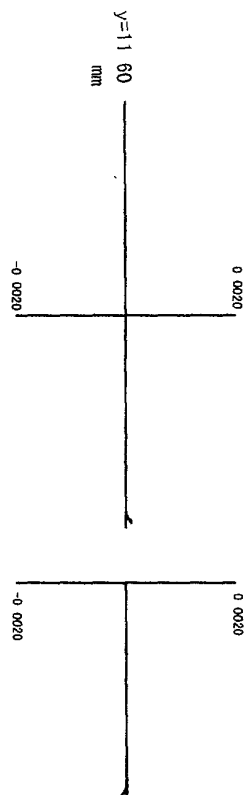
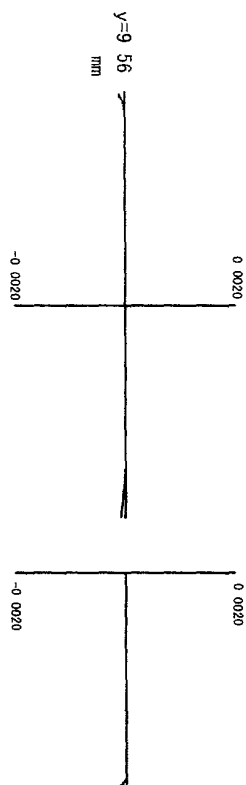


FIG. 40

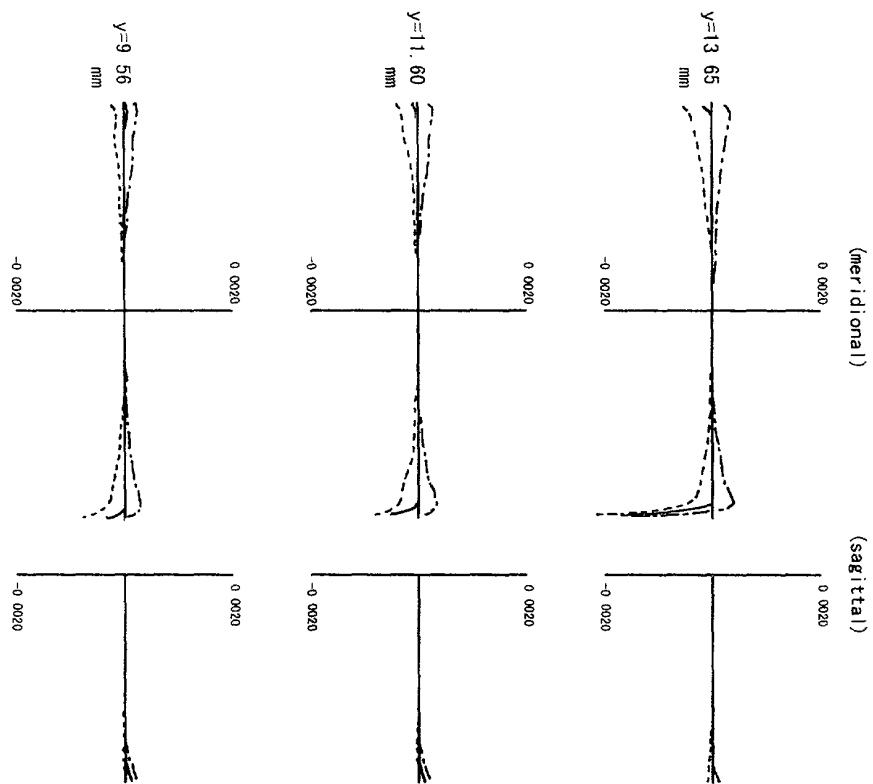
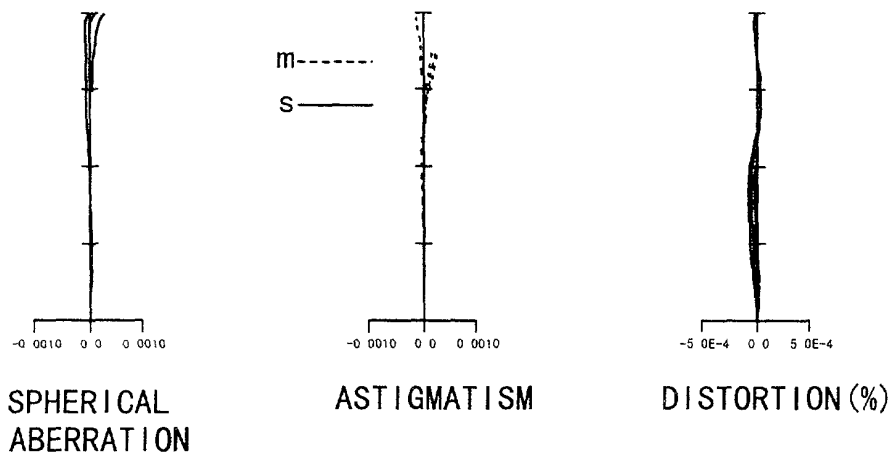
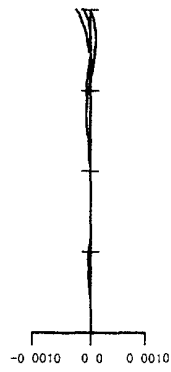
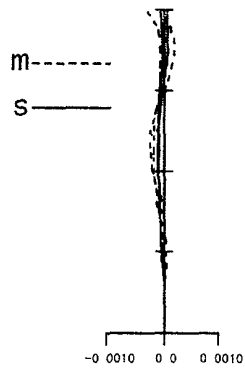


FIG. 41



SPHERICAL
ABERRATION



ASTIGMATISM



DISTORTION (%)

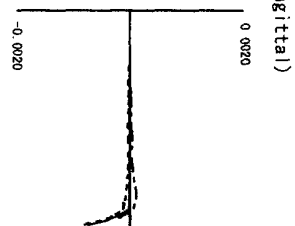
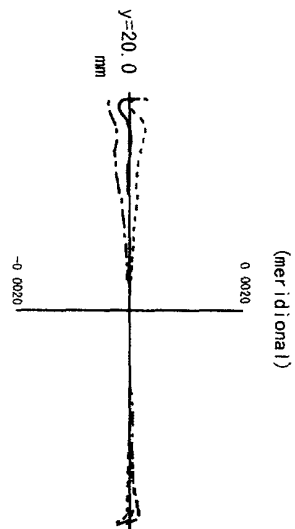
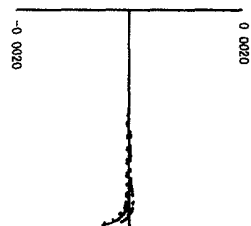
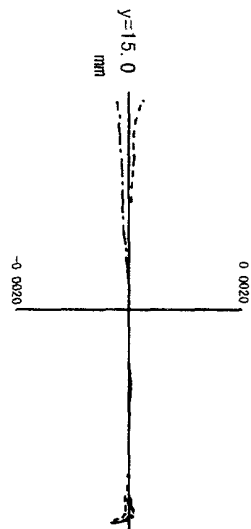
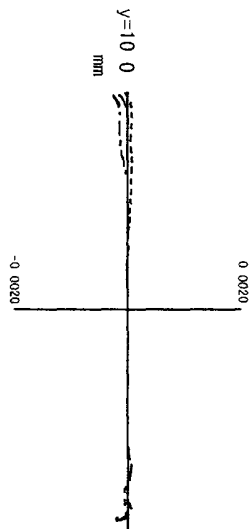
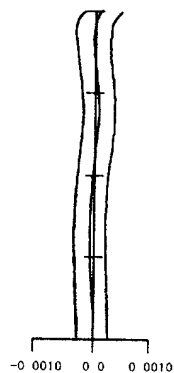
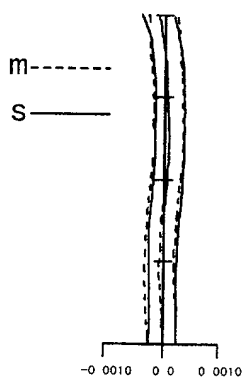


FIG. 42



SPHERICAL
ABERRATION



ASTIGMATISM



DISTORTION (%)

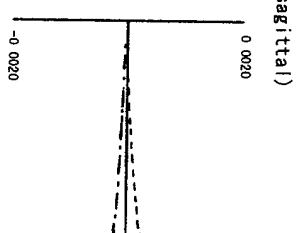
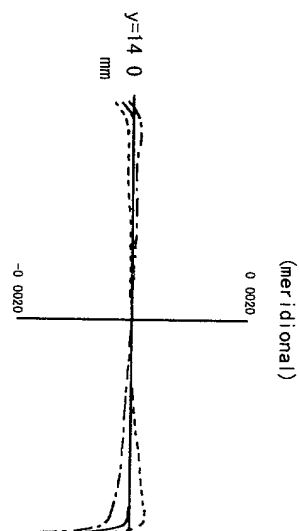
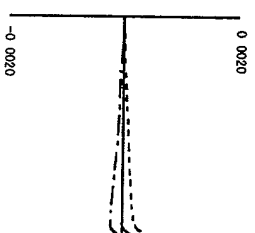
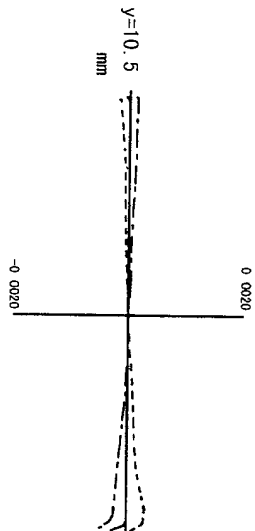
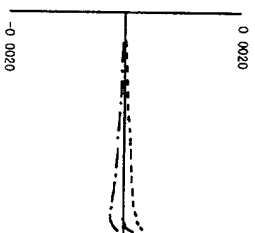
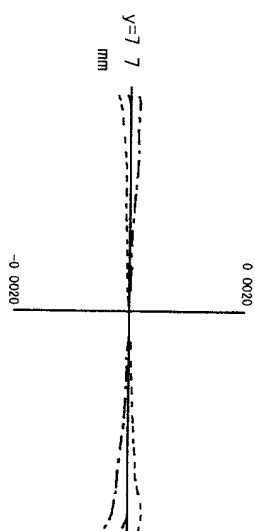
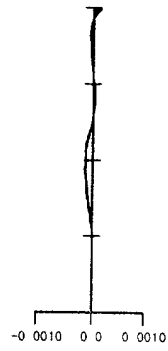
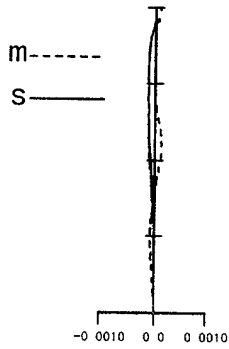


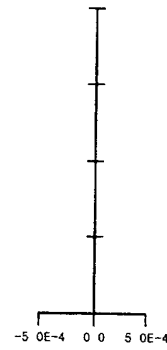
FIG. 43



SPHERICAL
ABERRATION



ASTIGMATISM



DISTORTION (%)

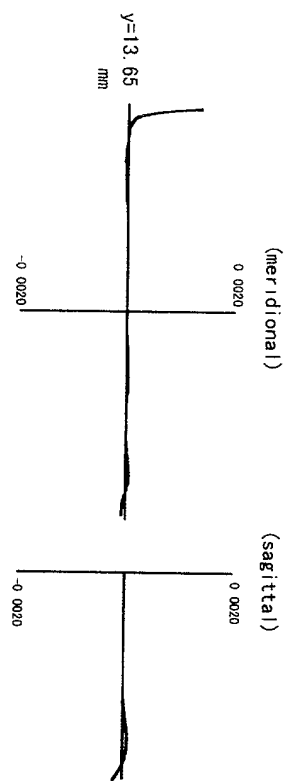
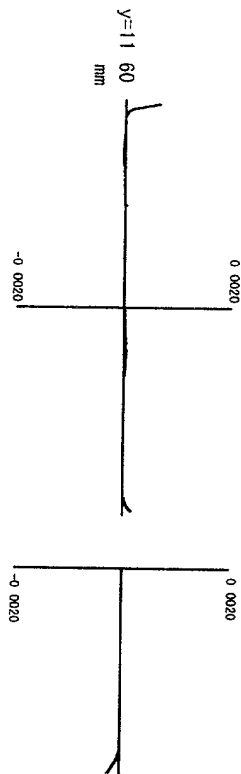
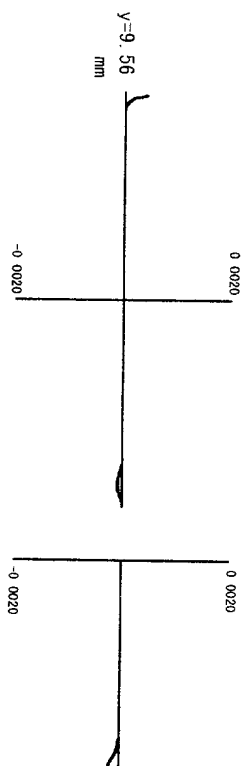


FIG. 44

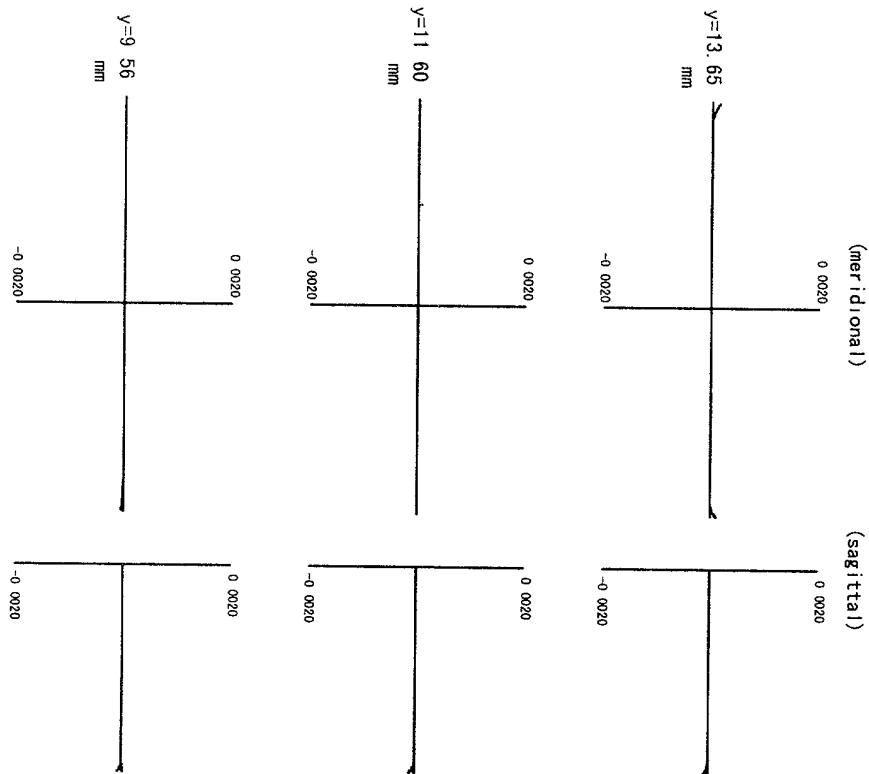
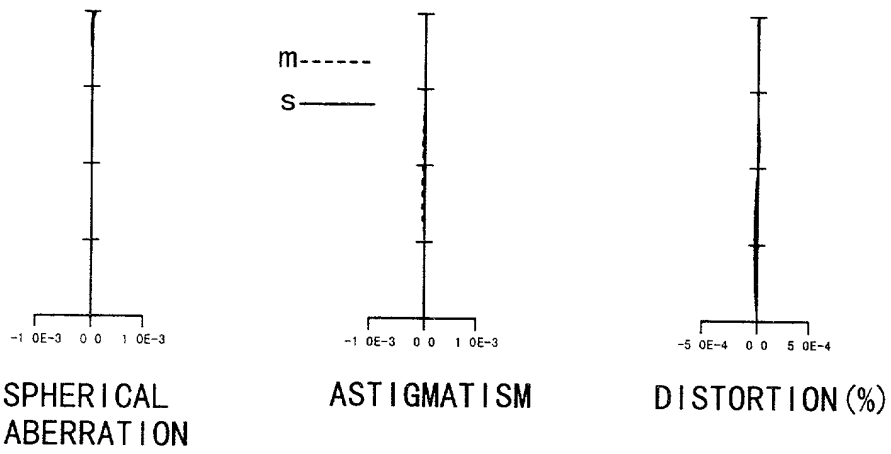


FIG. 45

NUMERICAL EXAMPLE NO.	1	2	3	4
BG2	-0.147	-0.127	-0.144	-0.234
BG1	-1.352	-1.443	-1.458	-0.857
P1	-0.015840	-0.013120	-0.016400	-0.005480
Pf+P2	0.015840	0.013120	0.016390	0.005490
e/LM1	0.977	1.113	0.976	0.930
01L/(LM1+2*LM2)	0.963	0.872	0.981	0.971
LM2/LM1	0.688	0.761	0.673	0.448
LM1/L	0.388	0.385	0.368	0.223
1/BGM1	-0.623	-0.851	-0.644	-0.490

NUMERICAL EXAMPLE NO.	5	6	7	8	9	10	11	12
BG2	-0.269	-0.204	-0.184	-0.192	-0.227	-0.121	-0.196	-0.199
BG1	-0.773	-0.779	-0.820	-0.944	-1.585	-1.358	-2.190	-2.318
P1	-0.010084	-0.009864	-0.008851	-0.009408	-0.009000	-0.013156	-0.008163	-0.008042
Pf+P2	0.010074	0.009881	0.008860	0.009393	0.008996	0.013159	0.008156	0.008036
e/LM1	1.100	1.038	2.414	1.771	0.909	0.943	0.803	0.797
01L/(LM1+2*LM2)	0.823	0.681	0.784	0.829	1.021	0.861	0.910	0.889
LM2/LM1	0.657	0.652	0.684	0.688	0.771	0.790	0.810	0.846
LM1/L	0.280	0.302	0.260	0.268	0.352	0.410	0.356	0.368
1/BGM1	-1.036	-1.792	-1.121	-0.972	-0.390	-0.809	-0.883	-0.876

FIG. 46

NUMERICAL EXAMPLE NO.	13	14	15	16	17	18	19	20	21
BG2	-0.122	-0.095	-0.141	-0.267	-0.193	-0.185	-0.153	-0.264	-0.280
BG1	-1.279	-1.250	-2.606	-3.838	-1.395	-2.071	-1.169	-36.671	-2.009
P1	-0.005007	-0.004643	-0.013843	-0.005904	-0.008983	-0.013972	-0.018751	-0.006985	-0.007175
Pf+P2	0.004999	0.004638	0.013836	0.005899	0.008986	0.013988	0.018743	0.006977	0.007171
e/LM1	1.164	1.088	0.914	0.959	1.113	0.925	1.000	1.316	0.979
01L/(LM1+2*LM2)	0.874	0.827	1.036	1.537	0.779	0.950	0.845	15.187	1.634
LM2/LM1	0.870	0.874	0.862	0.663	0.818	0.793	0.727	0.773	0.347
LM1/L	0.351	0.362	0.430	0.455	0.465	0.441	0.387	0.410	0.462
1/BGM1	-0.679	-0.778	-0.667	-0.670	-0.994	-0.796	-0.863	0.119	-0.551
LFM1/LFM2	0.565	0.650	0.745	0.595	0.716	0.556	0.522	0.569	0.602

FIG. 47